

# H₂S Scavenging: Amine Systems

This GATEKEEPER focuses on Amine Systems, one of the most commonly used regenerative H₂S scavengers in the Oil & Gas industry.

**Amine**

Amines are organic compounds derived from ammonia with substitution of one or all of the hydrogens with alkyl or aryl groups, retaining a basic nitrogen atom with one lone pair of electrons. They can be classified as Primary, Secondary, Tertiary, or Cyclic.

- Primary – One of three hydrogen atoms is replaced by alkyl or aryl groups
- Secondary – Two of the three hydrogen atoms are replaced by alkyl or aryl groups
- Tertiary – All three hydrogen atoms are replaced by alkyl or aryl groups
- Cyclic – Either secondary or tertiary amines with a cyclic structure with hydrogen atoms replaced by alkyl or aryl groups

**Amine Solution Selection**

The amine selected, as well as the concentration of the solution used, will result in different selectivity of H₂S over CO₂, mole-to-mole acid gas loading, and degradation of the amine. Blended solutions incorporating more than one amine, as well as specialty designed amine molecules, can be used to increase selectivity, loading, and degradation characteristics of the final solution. Typical operating ranges for common amines have been given in Table 1. Acid gas loading values are based on carbon-steel equipment; higher loading may be achievable with stainless steel or CRA systems.

Monoethanolamine (MEA), diethanolamine (DEA) and methyl diethanolamine (MDEA) are the most commonly used forms of amine in gas sweetening; although, disopropanolamine (DIPA) and aminoethoxyethanol/diglycolamine (DGA) are also used. All are aqueous solutions of alkylamines that are used to selectively strip H₂S and CO₂ from an acid-gas rich hydrocarbon gas stream.

**Monoethanolamine (MEA)**

MEA is commonly used in 15 – 20 weight % aqueous solutions. Due to corrosion issues, loading is limited to 0.30 – 0.35 moles acid gas per mole amine with carbon steel; loading as high as 0.70 – 0.90 mole/mole has been observed with stainless steel. Degradation products are extremely corrosive and should be removed via filters and reclaimer. Due to the high pH of MEA, all CO₂ will essentially be removed in the process of stripping H₂S to export specs.

**Diethanolamine (DEA)**

DEA, used in 25 – 35 weight % solutions, is also limited to 0.30 – 0.35 mole/mole loading in carbon steel, but can be loaded to 1 mole/mole when using stainless steel or corrosion inhibitors. Degradation products are less corrosive than MEA and reclamation is not practical due to the need for vacuum reclaimers. DEA has a lower affinity for CO₂ and H₂S and may not produce pipeline spec gas for some systems. Under low pressure and short residence time, DEA can be selective for H₂S over CO₂.

**Diglycolamine (DGA)**

DGA is usually used in 50 – 70 weight % solutions. Corrosion issues also prevent loading above 0.35 mole/mole. Preferentially selective for CO₂ over H₂S, but has a higher pH than MEA allowing it to reach pipeline specs unless gas stream has high CO₂ content. Higher solution strength results in reduced circulation rates and lower freezing point. DGA is also able to absorb COS, CS₂, SO₂, and SO₃.

<table>
<thead>
<tr>
<th>Amine</th>
<th>Solution (wt%)</th>
<th>Loading (mole / mole)</th>
<th>H₂S &gt; CO₂ Selectivity</th>
</tr>
</thead>
<tbody>
<tr>
<td>MEA</td>
<td>15 - 20</td>
<td>0.30 - 0.35</td>
<td>No</td>
</tr>
<tr>
<td>DEA</td>
<td>25 - 35</td>
<td>0.30 - 0.35</td>
<td>Limited</td>
</tr>
<tr>
<td>DGA</td>
<td>50 - 70</td>
<td>0.30 - 0.35</td>
<td>No</td>
</tr>
<tr>
<td>MDEA</td>
<td>20 - 50</td>
<td>0.70 - 0.80</td>
<td>Condition Dependent</td>
</tr>
</tbody>
</table>

Table 1: Amine Operating Ranges

**Figure 1: Primary Amine**

[Diagram of Primary Amine]

**Figure 2: Secondary Amine**

[Diagram of Secondary Amine]

**Figure 3: Tertiary Amine**

[Diagram of Tertiary Amine]
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Methyl Diethanolamine (MDEA)

Generally, MDEA is used in 20 – 50 weight % solutions, but lower weight % solutions have been used in very low pressure systems. Loading ranges of 0.70 – 0.80 can be achieved due to significantly reduced corrosion issues. Oxygen exposure will produce corrosive acids and can result in build-up of iron sulfide. MDEA is also selective towards H₂S over CO₂, has a lower vapour pressure, has lower heats of reaction, and has higher resistance to degradation compared to other amines.

Mixed Amines

Mixed amines are generally combinations of MDEA with DEA or MEA as up to 20% of the total amine. DEA or MEA are added to enhance the CO₂ removal where MDEA alone allows too much CO₂ to slip into the absorber or in low pressure systems where MDEA alone is unable to remove CO₂ to pipeline specs.

Amine Sweetening Process

The primary components of an amine sweetening system include:

- Contactor Tower
- Regeneration Tower
- Reboiler
- Heat Exchanger
- Condenser & Accumulator/Reflux Drum
- Makeup Tank

Optional components of an amine sweetening system include:

- Mechanical Filters
- Flash Tank
- Inlet Separator
- Charcoal Filters
- Reclaimer
- Outlet Separator

Filters can be used to remove solids & contaminants. An Inlet Separator may be used to remove hydrocarbons & water from the produced gas to reduce contaminants; an Outlet Separator may be used to remove any residual amine or solvent from the sweetened gas stream. A Flash Tank may be used to recapture hydrocarbons from the Rich amine. A Reclaimer unit is used for semi-continuous distillation with MEA solutions. DEA’s higher boiling temperature and lower degradation rate makes it less practical, less economical, and unnecessary to use a Reclaimer; filtration and caustic wash are sufficient purification for DEA.

Contactor Tower

The Lean (acid-gas free) amine is circulated from top to bottom over plates or packing as the produced gas to be sweetened enters from the bottom of the Tower.

By contact between the gas and the amine solution, acid gases (CO₂ & H₂S) are stripped into the amine solution. The sweetened produced gas exits the top of the tower; Rich (acid-gas containing) amine stream exits the bottom of the tower.

Heat Exchanger

Rich amine passes through the Heat Exchanger and is pre-heated by the hot regenerated Lean amine from the Reboiler. An optional Flash Tank for the Rich amine and Filters can be used on the Rich (Inlet) and Lean (Outlet) amine streams.

Regeneration Tower

Like the Contactor Tower, the Regeneration Tower is also filled with plates or packing. Heated Rich amine is fed into the top while steam and vapor from the Reboiler enter from the bottom. Acid-gas-rich vapor exits the top of the Tower to the Condenser and Lean amine leaves the bottom of the Tower, entering the Reboiler for further acid-gas stripping.

Reboiler

Heat is added at the Reboiler, generating steam and helping to break the chemical bonds between the amine and the acid gases. The CO₂ and H₂S-rich vapor is sent into the bottom of the Tower, where the lower partial pressure of the rising steam helps liberate acid gasses from the falling amine. Optionally, the Lean amine may be sent to a Reclaimer to remove contaminants such as salts.

Condenser & Accumulator/Reflux Drum

The acid-gas rich vapour from the Regeneration Tower is passed through a Condenser to drop water & any remaining amine, feeding into the Accumulator / Reflux Drum. The remaining acid-gas stream is sent for disposal; the water/amine solution is fed back into the top of the Regeneration Tower as reflux.

Makeup Tank

Some amine and solvent are lost due to heating, refluxing, and wetting of the gas stream; additionally, the amine in the selected solutions break down or degrade over repeated cycles and fall out as solids. Periodically, fresh amine solution from a Makeup Tank will have to be added to the system with the Lean amine stream.

Conclusion

A few key points should be considered before finalizing Amine System design and amine selection. Treated gas composition, including CO₂, H₂S, and other acid-gas contributors, must be understood to select the best amine for application. System pressures and re-circulation rates, as well as the use of stainless steel or a corrosion inhibitor, will impact amine selection, loading, and efficiency. Optional subsystems may improve performance and reduce degradation of the amine. For optimal operation and highest efficiency, all system components should be carefully selected.

References