

# Characterization of Nanoscale Surface Films in Solid Lubricants

Harmandeep S. Khare and David L. Burris (Advisor)  
University of Delaware, Department of Mechanical Engineering, Newark, Del.



Harman Khare is currently a doctoral candidate in the Materials Tribology Laboratory at the University of Delaware in Newark, Del., working under the mentorship of Dr. David Burris. His research interests include solid lubricants for extreme environments, surface characterization of solid lubricants and nanotribology. You can reach him at [khare@udel.edu](mailto:khare@udel.edu).

## INTRODUCTION

Extreme environments often preclude the use of conventional lubricants in moving mechanical systems. Molybdenum disulphide ( $\text{MoS}_2$ ), a lamellar solid lubricant exhibiting extremely low friction in vacuum, is often used to lubricate sliding interfaces in space applications.

Solid lubricants (particularly lamellar solids like  $\text{MoS}_2$ ) accommodate motion by forming sliding-induced low shear-strength surface films (called tribofilms). Though the conventional wisdom suggests a liquid-like bulk shear process, recent studies suggest that the films and shear are confined to within 10 nm of the surface.<sup>1</sup> These films have proven difficult to detect and even more difficult to probe mechanically.

The tribofilm is widely regarded as a critical element of low friction sliding. Understanding the tribology of solid lubrication requires an improved understanding of the tribofilm. The aims of this research are to (1.) investigate the effect of environment on evolution of a stable sliding interface and (2.) characterize the properties of these films at relevant length-scales to understand their contributions to macroscale friction and wear.

## EXPERIMENTAL

### Transient Wear

Transient wear and friction were measured using a custom-built tribometer with an optical interferometer (SWLI) positioned above the wear track (see Figure 1) to allow periodic wear measurements.

Six wear-rate measurements were made on one  $\text{MoS}_2$  coating (sputtered by Tribologix). The results are shown in Figure 2. The low initial wear rate of  $2 \times 10^{-8} \text{ mm}^3/(\text{Nm})$  increased by an order of magnitude after two subsequent tests in dry air (<500 PPM water). The wear rate in lab air (after dry testing) was higher by nearly another order of magnitude and tended to increase with subsequent testing over time.

We have consistently observed increased wear and friction (not shown) over time which suggests a time-dependent uptake of moisture into the bulk of the coating. To test this hypothesis, the sputtered coat-

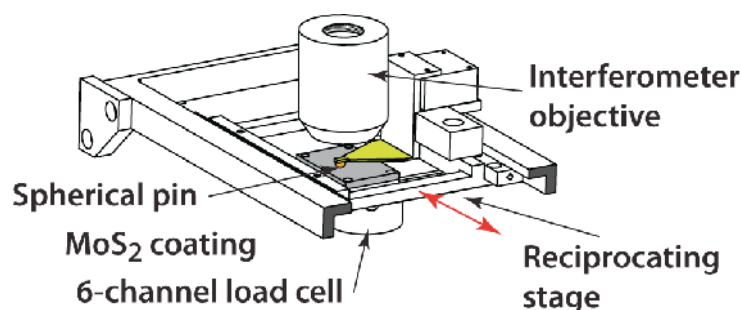


Figure 1 | Custom-tribometer used for measuring transient wear.

ing was annealed at 100°C for different durations and friction was measured after allowing the MoS<sub>2</sub> sample to cool to room temperature each time.

The friction coefficient (50 sliding cycles) decreases significantly with increased annealing time in between tests (see Figure 3). When the coating was annealed at 100°C for an hour, the friction coefficient in humid air at room temperature was comparable to those found in dry conditions. Similar measurements performed on hydrogenated diamond-like carbon (DLC) do not lead to any significant reduction in friction. During cooling, water adsorbs to the

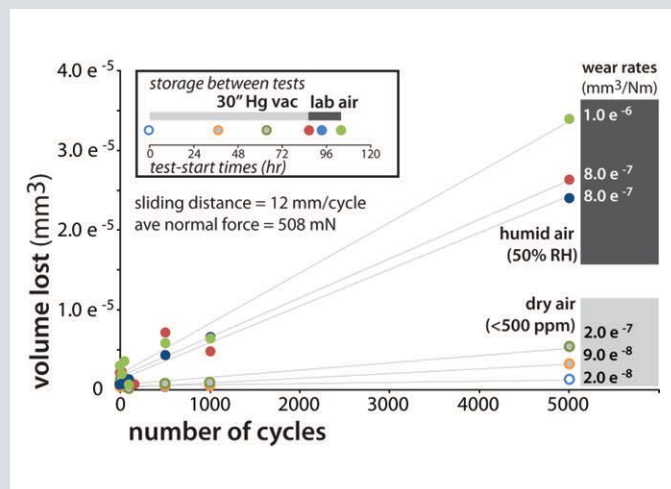


Figure 2 | Wear rates based on intermittent wear volume measurements for three dry sliding and three humid air wear tracks. Inset shows wait times between tests and corresponding coating storage condition.

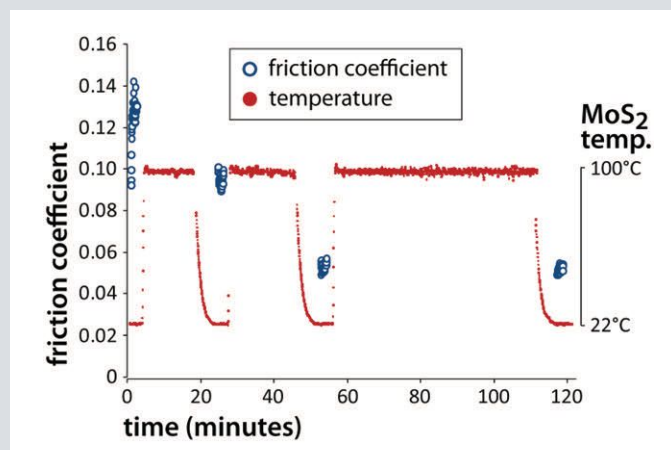


Figure 3 | Friction coefficient and temperature for annealing experiment. Each friction measurement of 50 sliding cycles (440 C against MoS<sub>2</sub>) was made in lab air at room temperature. Intervals of heating to 100°C in between tests reduced the amount of water in the coating, which led to reduced friction.

DLC surface and quickly reaches equilibrium with the environment. Conversely, friction of the MoS<sub>2</sub> coating remains low for several minutes in a humid environment after most of the water has been driven from the bulk. While DLC friction appears to be driven purely by coating surface adsorption (fast kinetics), bulk diffusion appears to play a significant role in the tribology of MoS<sub>2</sub> (see Figure 4).

### Nanotribology

To characterize tribofilms and their contribution in macroscale friction, a direct, yet non-invasive probe at the rel-

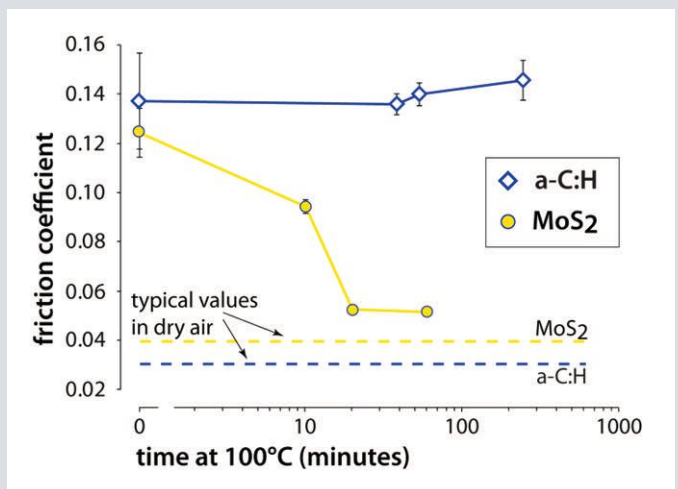


Figure 4 | A comparison of change in friction as function of annealing time for DLC and MoS<sub>2</sub> sputtered coatings in lab air. Intervals of heating between tests had no effect on DLC friction. Numbers within bars indicate number of measurements.

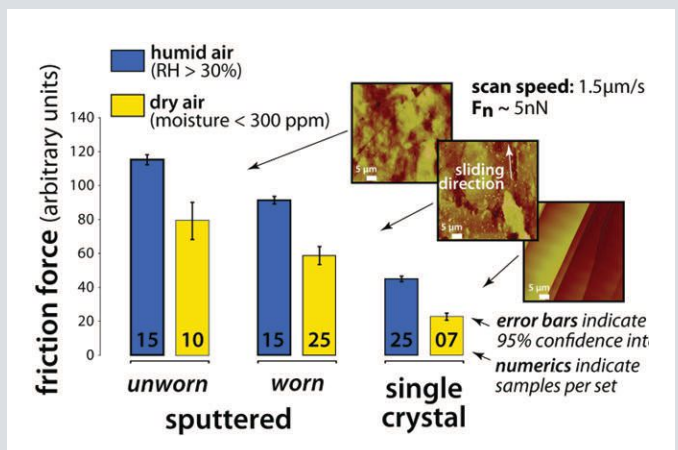


Figure 5 | Results for LFM measurements on sputtered and single crystal MoS<sub>2</sub> show both environmental and spatial correlation.

evant length-scales is required. Single-load lateral force microscopy measurements were performed with a silicon nitride tip on worn and unworn sputtered MoS<sub>2</sub> coatings and compared with single crystal MoS<sub>2</sub>.

As illustrated in Figure 5, nano-friction (quantified here by the width of friction loops) bore a direct correlation with the presence of moisture in the surrounding environment, irrespective of the substrate structure. Further, for similar environments, friction within the wear track is seen to be lower than for unworn MoS<sub>2</sub>, with the friction of single crystal MoS<sub>2</sub> being lowest in both environments.

These preliminary results illustrate the variation in nano-scale friction between worn and unworn sputtered coatings, presumably due to formation of ordered tribofilms and how these compares with the idealized single-crystal structure.

### CONCLUSIONS

- Transient wear measurements show moisture-dependence of MoS<sub>2</sub> wear across two distinct time-scales: the immediate environment and the coating 'exposure history,' suggesting effects of storage conditions on prevailing coating wear rate.

- Sensitivity of MoS<sub>2</sub> friction to annealing is seen as indicative of the tendency of MoS<sub>2</sub> to act as a sink for gradual moisture uptake over time, which during annealing is thermally driven out.
- Preliminary single-asperity measurements demonstrate that sliding-induced surface structure affects the frictional response and moisture sensitivity.

### ACKNOWLEDGMENTS

The authors gratefully acknowledge the AFOSR (YIP FA9550-10-1-0295) and the University of Delaware Research Foundation (UDRF) for their financial support.

### REFERENCES

1. Hu, J.J., Wheeler, R., Zabinski, J.S., Shade, P.A. and Shiveley, A. and Voevodin, A.A. (2008), "Transmission Electron Microscopy Analysis of Mo-W-S-Se Film Sliding Contact Obtained by Using Focused Ion Beam Microscope and In Situ Microtribometer," *Tribology Letters*, **32**(1), pp. 49-57.



Performance and service that are  
**LEADING EDGE**  
People and specialty products  
you can count on.

- SpectraSyn Ultra™ High VI Polyalphaolefin Base Oils Group IV
- SpectraSyn Plus™ Base Oils Group IV
- SpectraSyn™ Polyalphaolefin Base Oils Group IV
- Esterex™ Esters Group V
- Synesstic™ Alkylated Naphthalene Group V
- Ultra-S™ Base Oils Group III
- Pure Performance® Base Oils Group II
- ConoPure® Process Oils

7010 Mykawa | Houston, Texas 77033 | 800.228.3848 | [www.jamdistributing.com](http://www.jamdistributing.com)

Esterex, SpectraSyn, SpectraSyn Ultra and Synesstic are trademarks of Exxon Mobil Corporation. Ultra-S is a trademark and Pure Performance and ConoPure are registered by ConocoPhillips Company.

 Global Sales and Service

**J.A.M.**  
**SPECIALTY PRODUCTS**