

20 June 2024

KORSNÄS TSF EXPLORATION TARGET

Highlights

- Exploration Target based on 523 assay results from 57 drillholes from the Korsnäs Tailings Storage Facility (TSF)
- 480 assays of tailings material:
 - Average TREO¹: 6,465 ppm
 - Average NdPr Oxide²: 1,896 ppm
 - NdPr enrichment³: 29%
- 7 additional twinned holes reserved for metallurgical studies
- 12kg composite sample dispatched to BiotaTec in Estonia for proof-of-concept metallurgical tests

Next operations:

- Confirmatory diamond drilling in the main mine area, primarily for metallurgical test work
- Drill test the main targets at Korsnäs at least six REE mineralised structures identified by historic drilling
- Auger drilling of the lanthanide concentrate stockpile adjacent to the TSF
- Further assay results from historic drill core sampling are pending

The Korsnäs lead mine, located on Finland's west coast, was operational from 1958 to 1972. During this period, 0.87 million tonnes of ore were processed on-site at a recovered grade of 3.6% Pb, with tailings deposited in a dedicated Tailings Storage Facility (**TSF**) immediately north of the mine. Outokumpu, the original mine operator, was aware that the Korsnäs orebody contained Rare Earth Elements (**REEs**). Although an REE concentrate was produced on-site, it was never sold and remains stockpiled at the mine (the lanthanide concentrate stockpile). The REEs that were not recovered are now present in the TSF.

Prospech Limited (**Prospech** or the **Company**), through its wholly owned Finnish subsidiary Bambra Oy (**Bambra**), retains exploration tenure over the Korsnäs mine site, including the TSF and REE concentrate stockpile. The tenure also features at least six sub-parallel geological structures rich in REEs (the hard rock target). Prospech's exploratory efforts focus on investigating these structures, as well as the potential of the TSF and REE concentrate stockpile.

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¹ TREO = Total Rare Earth Oxides which is the sum of La₂O₃, CeO₂, Pr₆O₁₁, Nd₂O₃, Sm₂O₃, Eu₂O₃, Gd₂O₃, Tb₄O₇, Dy₂O₃, Ho₂O₃, Er₂O₃, Tm₂O₃, Yb₂O₃, Lu₂O₃ and Y₂O₃.

² NdPr Oxide = $Nd_2O_3 + Pr_6O_{11}$

³ NdPr enrichment % = NdPr Oxide / TREO

^{*}Refer Table 1

In early 2024, systematic testing of the TSF was conducted with 64 drill holes, reaching a combined total of 579 metres. A total of 523 samples were analysed for various elements, including the lanthanide series REEs. Bulk density determinations were completed on all samples.

The TSF was modelled in 3D using wireframes generated by combining Laser Imaging Detecting and Ranging (**LIDAR**) topography surfaces with surfaces derived from drilling information. Different assumptions regarding the composition of the TSF walls resulted in two models, representing upper and lower bound volume estimates. After bench compositing, the assay data was interpolated into a block model using an inverse-distance algorithm.

Despite the high-quality assay and spatial data, the TSF grade-tonnage estimate is classified as an Exploration Target until metallurgical test work, currently underway, demonstrates the likelihood of eventual economic extraction.

Tonnage Range Mt	TREO Range ppm	NdPr Oxide Range ppm	Nd ₂ O ₃ ppm	Pr ₆ O ₁₁ ppm	NdPr Enrichment %	Notes
0.93 –	6200 –	1800-	1400-	400-	29	Full Wall
0.72	6500	1880	1500	380	29	54° inner walls

The Korsnäs TSF Exploration Target, based on actual exploration results:

The potential quantity and grade are conceptual in nature. There has been insufficient exploration (including metallurgical test work) to estimate a Mineral Resource and it is uncertain if further exploration will result in the estimation of a Mineral Resource.

Location and Access

The Korsnäs REE project is located on Finland's west coast, near the Gulf of Bothnia (Figure 1). It is centred around a historic lead mine, situated 45 km southwest of Vaasa, 4 km northeast of Korsnäs, and 171 km from the significant port of Kokkola. The project is 700 km by road and vehicular ferry from the Neo Performance Materials REE processing facility in Narva, Estonia.

The main road between Vaasa and Korsnäs passes through the project area, which has access to grid power and communications. The REE TSF is just 700 metres from the main road (Figure 2).

Tenure

Tenure at Korsnäs comprises 4 tenements (Figure 3). The exploration licence called ML2021:0019 Hagg was granted by Tukes on 7 May 2024. This licence of 182.32 Ha covers the majority of the TSF. The entirety TSF is covered by an access agreement with the Korsnäs Community which provides access for exploration activities.

The remaining 3 tenements tenement areas are reserved by Reservation Notifications. Bambra will file for Exploration Permits approved by the Finnish Safety and Chemicals Agency (**TUKES**), the Finnish mining authority. Exploration Permit applications to be filed for handling by TUKES:

- VA2023:0040 Hägg 2 (185.55 Ha)
- VA2023:0083 Hägg 3 (167.15 Ha)
- VA2023:0093 Petalax (2,995.37 Ha)



Figure 1: Location of Korsnäs Project close to existing Battery Infrastructure in Western Finland.



Figure 2 Korsnäs TSF drill pattern and position near mine and main road.



Figure 3 Tenement package with control of most REE exposures in the Korsnäs area.

Historical Information

The Korsnäs lead mine, operational from 1958 to 1972, processed 0.87 Mt of ore on-site at a recovered grade of 3.6% Pb, with tailings deposited in a dedicated TSF located immediately north of the mine (refer to Figure 2).

Initially, when ore processing began in 1959, the primary focus lay on lead concentrate flotation. It wasn't until 1967 that REE concentrates were produced. According to records from the Geological Survey of Finland (**GTK**), it is likely that the first 366,000 tonnes of ore were processed before the REE flotation circuit was established. Following this, rare earth production experienced fluctuations, totalling approximately 504,000 tonnes of ore, while maintaining a recovered grade of about 0.75% rare earth oxides. The REE concentrate was not sold; instead, the majority has been preserved in a stockpile, which Prospech plans to subject to auger sampling in the near future.

Drilling

A total of 64 drill holes were completed, reaching a combined total of 579 metres (Table 1). The drilling was performed using a proprietary technique developed by the drilling contractor, Mitta Oy, specifically designed to recover saturated unconsolidated mine tailings. The drill holes were spaced at 40-metre intervals along north-south lines, with the drill lines themselves also spaced 40 metres apart. The holes were positioned in an offset manner along alternate drill lines, creating a diamond pattern (Figure 4).

Six of the holes were drilled as twins (denoted by hole numbers with the suffix "A") to evaluate the consistency of results over short distances. Samples were collected at 1-metre intervals for all drill holes, except near the base of the TSF where a distinct change in material type was observed; in these cases, samples of less than 1 metre were collected. Seven holes were drilled specifically for metallurgical testing twins (denoted by hole numbers with the suffix "M"), with samples from these holes sealed and retained on site for future analysis.



Figure 4 Korsnäs TSF drilling.

Table 1 Assayed Drillhole Specifications

	EAST	NORTH	RL	FINAL_DEPTH		EAST	NORTH	RL	FINAL_DEPTH
	m	m	m	m	HOLE_ID	m	m	m	m
TSF01	206,532.20	6,978,120.02	12.11	8.00	TSF24	206,690.00	6,978,120.10	11.38	12.00
TSF02	206,530.15	6,978,160.08	12.08	9.10	TSF25	206,681.04	6,978,159.92	11.24	8.00
TSF03	206,529.11	6,978,201.59	11.77	9.00	TSF25A	206,680.59	6,978,157.31	11.20	9.00
TSF04	206,527.55	6,978,240.81	12.36	10.00	TSF26	206,685.00	6,978,200.04	11.46	8.00
TSF05	206,529.74	6,978,280.55	12.31	9.00	TSF27	206,686.58	6,978,240.82	11.61	10.00
TSF06	206,569.27	6,978,099.66	11.92	9.00	TSF28	206,690.39	6,978,279.80	12.19	10.00
TSF07	206,569.60	6,978,138.12	11.60	9.00	TSF29	206,728.90	6,978,065.61	11.59	10.00
TSF08	206,570.65	6,978,179.78	11.73	8.00	TSF30	206,729.85	6,978,100.69	11.80	9.00
TSF08A	206,570.30	6,978,181.47	11.73	9.00	TSF31	206,727.97	6,978,139.80	11.31	8.00
TSF09	206,569.28	6,978,220.09	11.63	8.00	TSF32	206,730.91	6,978,259.77	11.58	9.00
TSF10	206,567.90	6,978,259.55	11.91	8.00	TSF33	206,731.39	6,978,220.37	11.29	10.00
TSF11	206,568.82	6,978,293.63	12.35	9.00	TSF34	206,809.71	6,978,062.47	11.83	10.00
TSF12	206,608.50	6,978,082.54	11.68	9.00	TSF35	206,773.55	6,978,075.67	11.72	9.00
TSF13	206,611.41	6,978,119.88	11.62	9.00	TSF36	206,770.08	6,978,119.99	11.49	9.00
TSF14	206,610.45	6,978,160.80	11.36	8.00	TSF37	206,770.02	6,978,159.91	11.35	9.00
TSF14A	206,608.88	6,978,162.70	11.35	9.00	TSF38	206,770.01	6,978,199.64	11.17	10.00
TSF15	206,609.93	6,978,199.80	11.40	8.00	TSF39	206,769.19	6,978,240.93	11.64	10.00
TSF16	206,610.03	6,978,240.06	11.73	7.00	TSF40	206,769.75	6,978,279.93	11.80	10.00
TSF16A	206,611.08	6,978,237.97	11.66	8.00	TSF41	206,808.33	6,978,062.82	11.63	10.00
TSF17	206,610.05	6,978,279.88	11.92	9.00	TSF42	206,809.49	6,978,102.60	11.84	9.00
TSF18	206,649.60	6,978,097.50	11.83	9.00	TSF43	206,812.09	6,978,139.56	11.86	9.00
TSF19	206,650.08	6,978,139.89	11.37	9.00	TSF44	206,812.76	6,978,180.52	11.68	10.00
TSF20	206,639.05	6,978,179.95	11.43	7.00	TSF45	206,810.51	6,978,217.78	11.77	9.00
TSF20A	206,639.32	6,978,177.83	11.32	8.00	TSF46	206,808.37	6,978,262.14	11.87	10.00
TSF21	206,649.57	6,978,226.41	11.32	8.00	TSF47	206,810.43	6,978,288.33	12.27	10.00
TSF22	206,650.23	6,978,259.39	11.93	9.00	TSF48	206,841.89	6,978,121.17	12.35	10.00
TSF23	206,689.81	6,978,078.30	11.78	9.00	TSF49	206,847.08	6,978,159.82	12.38	10.00
TSF23A	206,689.85	6,978,076.16	11.61	9.10	TSF50	206,849.75	6,978,197.28	12.40	11.00
TSF24	206,690.00	6,978,120.10	11.38	12.00	TSF51	206,851.71	6,978,223.83	12.25	11.00

Sampling and Assaying

Samples were double-bagged and sealed in heavy duty plastic bags to retain the original moisture content of the TSF material. These samples were dispatched by road to the ALS laboratory in Outokumpu. The assay suite, including the ALS methods and detection limits, is detailed in Table 2.

ALS method ME-MS81h, which involves lithium borate fusion with ICP-MS analysis, is suitable for oregrade rare REEs. Additionally, method ME-ICP61 uses a four-acid digestion on a 0.25g sample, followed by ICP-AES analysis was used for other elements.

ALS Method	Element	Units	Detection Limit	ALS Method	Element	Units	Detection Limit
ME-MS81h	Ce	ppm	3	ME-ICP61	Ag	ppm	0.5
ME-MS81h	Dy	ppm	0.3	ME-ICP61	Al	%	0.01
ME-MS81h	Er	ppm	0.2	ME-ICP61	As	ppm	5
ME-MS81h	Eu	ppm	0.2	ME-ICP61	Ba	ppm	10
ME-MS81h	Gd	ppm	0.3	ME-ICP61	Be	ppm	0.5
ME-MS81h	Hf	ppm	1	ME-ICP61	Bi	ppm	2
ME-MS81h	Ho	ppm	0.05	ME-ICP61	Ca	%	0.01
ME-MS81h	La	ppm	3	ME-ICP61	Cd	ppm	0.5
ME-MS81h	Lu	ppm	0.05	ME-ICP61	Со	ppm	1
ME-MS81h	Nb	ppm	1	ME-ICP61	Cr	ppm	1
ME-MS81h	Nd	ppm	0.5	ME-ICP61	Cu	ppm	1
ME-MS81h	Pr	ppm	0.2	ME-ICP61	Fe	%	0.01
ME-MS81h	Rb	ppm	1	ME-ICP61	Ga	ppm	10
ME-MS81h	Sm	ppm	0.2	ME-ICP61	K	%	0.01
ME-MS81h	Sn	ppm	5	ME-ICP61	La	ppm	10
ME-MS81h	Та	ppm	0.5	ME-ICP61	Li	ppm	10
ME-MS81h	Tb	ppm	0.05	ME-ICP61	Mg	%	0.01
ME-MS81h	Th	ppm	0.3	ME-ICP61	Mn	ppm	5
ME-MS81h	Tm	ppm	0.05	ME-ICP61	Mo	ppm	1
ME-MS81h	U	ppm	0.3	ME-ICP61	Na	%	0.01
ME-MS81h	W	ppm	5	ME-ICP61	Ni	ppm	1
ME-MS81h	Y	ppm	3	ME-ICP61	Р	ppm	10
ME-MS81h	Yb	ppm	0.2	ME-ICP61	Pb	ppm	2
ME-MS81h	Zr	ppm	10	ME-ICP61	S	%	0.01
				ME-ICP61	Sb	ppm	5
				ME-ICP61	Sc	ppm	1
				ME-ICP61	Sr	ppm	1
				ME-ICP61	Th	ppm	20
				ME-ICP61	Ti	%	0.01
				ME-ICP61	Tl	ppm	10
				ME-ICP61	U	ppm	10
				ME-ICP61	V	ppm	1
				ME-ICP61	W	ppm	10
				ME-ICP61	Zn	ppm	2

Table 2 Analytical methods and detection limits

Density

Density was determined at ALS using method OA-GRA09. This parameter is measured by submerging a sample in water to determine the volume of water displaced. The sample's weight is then divided by the displaced water volume to calculate the density in g/cm³. Afterward, the sample is dried, and the dry weight is divided by the original volume to determine the Dry Bulk Density (**DBD**).

QA-QC

Standard reference materials, duplicates, and blanks were not inserted into the sample stream due to the lack of readily available materials. To mitigate, six twin holes were drilled to serve as field duplicates (Figure 5), and coarse rejects are currently being sent for analysis at a different laboratory. Internal ALS laboratory assays of blanks, standards, and duplicates did not reveal any significant issues.



Figure 5 Cross sections: Comparison of TREO assays of six pairs of twinned holes from TSF.

Statistics

The basic statistics for the element suite (REEs converted to oxides) and DBD and calculated quantities TREO⁴, LREO⁵, HREO⁶ and Nd+Pr_Oxide⁷ for all 523 assayed samples are presented in Table 3. This table includes 43 assays of non-tailings material at the base of the TSF. Restricting to 480 tailings samples, Figure 6 and 7 show histograms for Neodymium Oxide and Praseodymium Oxide distributions.

⁴ TREO = Total Rare Earth Oxides which is the sum of La₂O₃, CeO₂, Pr₆O₁₁, Nd₂O₃, Sm₂O₃, Eu₂O₃, Gd₂O₃, Tb₄O₇, Dy₂O₃, Ho₂O₃, Er₂O₃, Tm₂O₃, Yb₂O₃, Lu₂O₃ and Y₂O₃

⁵ LREO = Light Rare Earth Oxides which is the sum of La₂O₃, CeO₂, Pr₆O₁₁, Nd₂O₃, Sm₂O₃, Eu₂O₃, Gd₂O₃,

⁶ HREO = Total Rare Earth Oxides which is the sum of Tb₄O₇, Dy₂O₃, Ho₂O₃, Er₂O₃, Tm₂O₃, Yb₂O₃, Lu₂O₃ and Y₂O₃

⁷ Nd+Pr Oxide = Nd₂O₃ + Pr₆O₁₁



Figure 6 Distribution of TREO from 480 TSF drilling samples, Average = 6,465 ppm.



Figure 7 Distribution of Neodymium Oxide from 480 TSF drilling samples, Average = 1,518 ppm.

Table 3 Basic sample statistics

Field Name	Minimum	Maximum	No of Points	Mean	Std Dev
	250.00	17 934 00	523	5 007 22	2 006 11
IREO	211.00	17 286 00	523	5 765 53	2,550.11
HREO	34 70	647.60	523	231.66	105 21
Nd+Pr Oxide npm	52.85	5,540,90	523	1,756,94	919.44
La2O3_nnm	44 57	2 791 74	523	1 034 70	488 58
CeO2 npm	98.24	7 687 28	523	2 578 59	1 285 49
Pr6O11 ppm	10.99	1.075.12	523	350.09	180.17
Nd2O3 ppm	41.86	4.465.78	523	1.406.85	739.60
Sm2O3_ppm	7.54	731.96	523	224.59	118.72
Eu2O3 ppm	1.51	157.49	523	51.70	26.47
Gd2O3 ppm	6.00	377.03	523	119.04	61.20
Tb4O7 ppm	0.79	34.57	523	11.10	5.63
Dy2O3_ppm	4.25	119.97	523	40.43	19.86
Ho2O3_ppm	0.83	16.16	523	5.58	2.59
Er2O3_ppm	2.29	30.40	523	11.29	4.98
Tm2O3_ppm	0.25	3.15	523	1.20	0.49
Yb2O3_ppm	1.82	16.06	523	6.29	2.36
Lu2O3_ppm	0.26	1.84	523	0.83	0.29
Y2O3_ppm	24.13	425.45	523	154.94	69.21
Ag_ppm	0.25	17.00	523	0.44	0.78
Al_pcnt	3.95	7.66	523	5.91	0.68
As_ppm	2.50	34.00	523	9.45	5.28
Ba_ppm	170.00	10,100.00	523	4,963.35	3,205.54
Be_ppm	1.00	3.20	523	2.05	0.38
Bi_ppm	1.00	76.00	523	23.09	13.45
Ca_pcnt	1.24	11.95	523	5.58	2.42
Cd_ppm	0.25	16.10	523	4.20	1.89
Co_ppm	1.00	41.00	523	7.94	3.51
Cr_ppm	27.00	111.00	523	54.78	9.98
Cu_ppm	11.00	115.00	523	25.70	10.45
Fe_pcnt	2.01	6.05	523	3.50	0.79
Ga_ppm	10.00	20.00	523	12.64	4.41
Hf_ppm	1.00	7.00	523	2.68	1.06
K_pcnt	1.83	5.65	523	3.32	0.63
Li_ppm	20.00	80.00	523	41.74	13.31
Mg_pcnt	0.69	5.00	523	2.72	0.94
Mn_ppm	303.00	1,295.00	523	834.48	180.58
Mo_ppm	0.50	5.00	523	2.35	0.99
Na_pcnt	0.44	2.35	523	1.0/	0.36
Nb_ppm	4.00	19.00	523	10.24	1.94
NI_ppm	15.00	2/3.00	523	81.12	30.17
P_ppm	530.00	10,100.00	523	4,657.11	1,889.91
Pb_ppm	63.00	14,800.00	523	4,648.13	2,282.86
Kb_ppm	48.00	107.00	523	111.85	21.04
S_pcnt	0.04	2.08	523	0.55	0.30
So_ppm	2.50	14.00	523	2.52	1.42
Sc_ppin	3.00	7.00	523	7.90	1.45
Sn_ppm	2.50	7.00	523	2.30	1.016.61
Ji_ppili Ta_ppm	223.00	3,130.00	523	2,040.85	1,010.01
Ta_ppin Th_ppm	8 20	252.00	523	76.42	/1 29
Ti nont	0.00	0.40	523	0.42	0.04
TL nom	5.00	10.40	523	5 1/	0.04
U ppm	3.00	231.00	523	67.02	42 79
V nnm	45.00	192.00	525	96.49	21.70
W nnm	2 50	20 00	522	2 62	1 27
Zn nnm	48.00	2 2 2 0 00	523	2.00	177 52
Zr ppm	30.00	2,220.00	523	101 47	41 69
DBD	0.06	200.00	523	1 27	0.25
	0.00	2.11	525	1.2/	0.20

3D Modelling

Understanding the composition of the TSF walls is critical for accurate grade and volume estimates. Historical drawings indicate that the TSF walls were constructed in two lifts using a downstream design. However, there is no available historical information regarding the actual composition of the walls. Contemporary drilling data suggests that the walls were constructed from de-watered tailings. **Upper Bound Estimate:** Assumes the TSF walls are composed of tailings and includes them in the estimate.

Lower Bound Estimate: Assumes the walls are waste material with an inner slope from the crest of 54 degrees.

The 3D modelling process proceeded as follows:

1. Defining the Base: The base of the TSF was defined by lithology and assays from each drill hole. A gridded surface was then constructed from these points using Micromine Origin software.

2. Defining the Outer Walls and Top: The outer walls and top of the TSF were defined using LIDAR DTM data.

3. Creating Sectional Strings: North-south oriented sectional slices were created at 10-metre eastwest intervals for the defined surfaces, covering the extent of the TSF. Closed strings were digitized for each section, connecting the base and the top/sides.

4. Creating the 3D Wireframe: These 10-metre spaced closed strings were used to create a 3D wireframe, enclosing the contents of the TSF.

This procedure was carried out twice, once for the upper bound and once for the lower bound estimates described above.

Block Modelling

A block model was created in Micromine.

Table 4 Block Modelling Limits

Extents						
	Min centre	Block size	Max centre			
East	206490	20	206870			
North	6978030	20	6978330			
Z	-1	1	12			

The creation of the block model was constrained by the 3D wireframe described above. Sub-blocking was enabled to more accurately honour the 3D wireframe boundaries. The minimum sub-block size was 5 metres in the East and West directions and 0.5 metres in the Z (RL) direction. The highly anisotropic nature of the block model and the interpolation ellipsoid was justified, considering the expected spatial continuity of the tailings that were deposited as a series of nearly flat-lying beaches.



Figure 8 Korsnäs TSF Cross Section with block model TREO grades



Figure 9 Korsnäs TSF level flitch plan with block model TREO grades

Compositing

Assays were composited on 1 metre "benches". The 1 metres interval used reflects the dominant 1 metres sampling interval in the drilling.

Interpolation

Grades and DBD were interpolated into the block model using an inverse distance (1/D) algorithm. All elements in the database were interpolated in a single pass using a search ellipsoid with the following semi-axes (East = North = 40m, X = 0.5m)

Other interpolation parameters were:

Sectors	One sector	~
Max points per sector	6	
Min points (total)	1	

The results of the block modelling are depicted in Figure 9 which is a typical cross section through the centre of the TSF and Figure 10 which is a typical flitch plan at 7m RL.

Two interpolated models were created, one for the upper bound and one for the lower bound estimates described above.

Model Validation

The Block model was validated by visual inspection on a section by section basis and good agreement was observed between the model values and the original drill holes. See Figure 11 for a typical example.

In addition to the 1/D interpolation a nearest neighbour (NN) interpolation was carried out on the key quantity (TREO). The difference between the 1/D and NN grades was only 8 ppm (0.1%).



Figure 10 Korsnäs TSF Cross Section comparing grade composite and block model TREO grades

The histogram of the original sample values was compared with the histogram of the block values. The mean of both distributions were acceptably close. The standard deviation of the block distribution was lower, as expected.



Figure 11 Histograms comparing grade composite and block model TREO grades

Estimate Classification

The estimate is clearly defined in terms of grade and tonnage to the lower bound estimate. However, insufficient metallurgical work has been done to show reasonable prospects of eventual economic extraction of the REEs in this deposit. As a result, it is not classified as a mineral resource under JORC (2012). Instead, this estimate is classified as an Exploration Target.

Grade Tonnage Relationship

Figure 12 below depicts the TREO grade-tonnage for various TREO cut off grades (upper boundary case incorporating the entire TSF walls).



Figure 12: TSF modelled grade-tonnage curves

Additional Work Program

The activities planned for 2024 aim to improve the status of the current exploration target to a mineral resource estimate. The work program includes:

- Auger sampling of the outer TSF wall to determine the type of material it comprises and its REE content.
- Completion of sighter and proof-of-concept metallurgical tests currently underway at BiotaTec in Estonia.
- Completion of additional metallurgical tests, likely at GTK-Mintek laboratory in Finland.

Competent Person Statement

The information in this Report that relates to Exploration Results and the JORC Exploration Target is based on information compiled by Mr John Levings, who is a Fellow of the Australasian Institute of Mining and Metallurgy. Mr Levings, who is Executive Director – Technical of the Company, has sufficient experience which is relevant to the style of mineralisation and type of deposit under consideration and to the activity which he is undertaking to qualify as a Competent Person as defined in the 2012 edition of the 'Australasian Code for Reporting of Exploration Results, Exploration Targets, Mineral Resources and Ore Reserves'. Mr Levings consents to the inclusion in this Report of the matters based on the information in the form and context in which it appears.

The potential quantity and grade of this exploration target is conceptual in nature, there is currently insufficient exploration completed to support a mineral resource of this size and it is uncertain whether continued exploration will result in the estimation of a JORC resource. The Exploration Target has been prepared in accordance with the JORC Code (2012).

Section 1 Sampling Techniques and Data

Criteria	JORC Code explanation	Commentary
Sampling techniques	Nature and quality of sampling (eg cut channels, random chips, or specific specialised industry standard measurement tools appropriate to the minerals under investigation, such as down hole gamma sondes, or handheld XRF instruments, etc). These examples should not be taken as limiting the broad meaning of sampling. Include reference to measures taken to ensure sample representivity and the appropriate calibration of any measurement tools or systems used. Aspects of the determination of mineralisation that are Material to the Public Report. In cases where 'industry standard' work has been done this would be relatively simple (eg 'reverse circulation drilling was used to obtain 1 m samples from which 3 kg was pulverised to produce a 30 g charge for fire assay'). In other cases more explanation may be required, such as where there is coarse gold that has inherent sampling problems. Unusual commodities or mineralisation types (eg submarine nodules) may warrant disclosure of detailed information.	Sampling was carried out using a drilling system, purpose- designed for sampling tailings and owned by Mitta OY.
Drilling techniques	Drill type (eg core, reverse circulation, open-hole hammer, rotary air blast, auger, Bangka, sonic, etc) and details (eg core diameter, triple or standard tube, depth of diamond tails, face-sampling bit or other type, whether core is oriented and if so, by what method, etc).	The drill bit was of hardened steel and use spring steel metal fingers to retain the unconsolidated sample inside a hollow sampling tube. Compressed air was used to prevent sample entering the collection tube until the top of the desired interval was reached
Drill sample recovery	Method of recording and assessing core and chip sample recoveries and results assessed. Measures taken to maximise sample recovery and ensure representative nature of the samples. Whether a relationship exists between sample recovery and grade and whether sample bias may have occurred due to preferential loss/gain of fine/coarse material.	the weight of each sample was recorded. Weights and moisture content were variable. Six pairs of twinned holes gave good correlations suggesting that bias is not a factor
Logging	Whether core and chip samples have been geologically and geotechnically logged to a level of detail to support appropriate Mineral Resource estimation, mining studies and metallurgical studies. Whether logging is qualitative or quantitative in nature. Core (or costean, channel, etc) photography. The total length and percentage of the relevant intersections logged.	the sample was logged as either tailings or original surface from the base of the TSF
Sub-sampling techniques and sample preparation	If core, whether cut or sawn and whether quarter, half or all core taken. If non-core, whether riffled, tube sampled, rotary split, etc and whether sampled wet or dry. For all sample types, the nature, quality and appropriateness of the sample preparation technique. Quality control procedures adopted for all sub- sampling stages to maximise representivity of samples. Measures taken to ensure that the sampling is representative of the in situ material collected, including for instance results for field duplicate/second-half sampling. Whether sample sizes are appropriate to the grain size of the material being sampled.	The whole of the sample was assayed – no sub sampling At this early stage no QC samples have been collected. PRS intends to carry out umpire lab checks on both laboratory pulps and coarse crush rejects
Quality of assay data and laboratory tests	The nature, quality and appropriateness of the assaying and laboratory procedures used and whether the technique is considered partial or total. For geophysical tools, spectrometers, handheld XRF instruments, etc, the parameters used in determining the analysis including instrument make and model, reading times, calibrations factors applied and their derivation, etc. Nature of quality control procedures adopted (eg	Assays were be carried out by ALS, an internationally certified commercial laboratory following standard procedures (ALS method ME-MS81h for REEs). PRS inserted standards and blanks were not used due to the lack of ready availability of suitable reference materials for REEs. ALS has its own system of standard and blanks which were reported to PRS and showed no issues. This lack was mitigated by the cross referencing a large numbers of samples with readings from a hand-held pXRF analyser. On average the ALS

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	standards, blanks, duplicates, external laboratory checks) and whether acceptable levels of accuracy (ie lack of bias) and precision have been established.	results for La Ce Nd and Pr were ~10% lower than the pXRF readings. It is PRS's plan to submit pulps and coarse rejects to a second commercial laboratory for additional assaying and comparison of REE concentrations.
Verification of sampling and assaying	The verification of significant intersections by either independent or alternative company personnel. The use of twinned holes. Documentation of primary data, data entry procedures, data verification, data storage (physical and electronic) protocols. Discuss any adjustment to assay data.	Six pairs of twinned holes were drilled and assays. Results show good correspondence between the holes. Rare Earth Oxide values were calculated from chemical formulas and atomic weights.
Location of data points	Accuracy and quality of surveys used to locate drill holes (collar and down-hole surveys), trenches, mine workings and other locations used in Mineral Resource estimation. Specification of the grid system used. Quality and adequacy of topographic control.	Mitta OY used an DGPS to survey the collar locations of the holes in the ETRS-TM35FIN projection (EPSG:3067).
Data spacing and distribution	Data spacing for reporting of Exploration Results. Whether the data spacing and distribution is sufficient to establish the degree of geological and grade continuity appropriate for the Mineral Resource and Ore Reserve estimation procedure(s) and classifications applied. Whether sample compositing has been applied.	Spacing of the drillholes was 40m N-S along staggered sections 40m apart E-W (See Figure 1) Downhole sample were collected continuously every 1 metre
Orientation of data in relation to geological structure Sample security	Whether the orientation of sampling achieves unbiased sampling of possible structures and the extent to which this is known, considering the deposit type. If the relationship between the drilling orientation and the orientation of key mineralised structures is considered to have introduced a sampling bias, this should be assessed and reported if material. The measures taken to ensure sample security.	No bias is believed to be introduced by the sampling method. Samples were sealed securely in double plastic bag and kept in a secure area until despatch to the laboratory by professional courier
Audits or reviews	The results of any audits or reviews of sampling techniques and data.	No audits or reviews of the data management system have been carried out.

Section 2 Reporting of Exploration Results

Criteria	JORC Code explanation	Commentary
Mineral tenement and land tenure status	Type, reference name/number, location and ownership including agreements or material issues with third parties such as joint ventures, partnerships, overriding royalties, native title interests, historical sites, wilderness or national park and environmental settings. The security of the tenure held at the time of reporting along with any known impediments to obtaining a license to operate in the area.	Prospech Limited has 100% interest in Bambra Oy ('Bambra'), a company incorporated in Finland. The laws of Finland relating to exploration and mining have various requirements. As the exploration advances specific filings and environmental or other studies may be required. There are ongoing requirements under Finnish mining laws that will be required at each stage of advancement. Those filings and studies are maintained and updated as required by Prospech's environmental and permit advisors specifically engaged for such purposes. The Company is the manager of operations in accordance with generally accepted mining industry standards and practices. The Korsnäs project's tenure is secured by Exploration Permit Application Number ML2021:0019 Hägg and Reservation Notification VA2023:0040 Hägg 2.
Exploration done by other parties	Acknowledgment and appraisal of exploration by other parties.	The area of Korsnäs has been mapped, glacial till boulder sampled and drilled by private companies including and Outokumpu Oy.
Geology	Deposit type, geological setting and style of mineralisation.	The historic Korsnäs Mine deposited tailing in the TSF approximately 760,000t

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Drill hole Information	A summary of all information material to the understanding of the exploration results including a tabulation of the following information for all Material drill holes: easting and northing of the drill hole collar elevation or RL (Reduced Level – elevation above sea level in metres) of the drill hole collar dip and azimuth of the hole down hole length and interception depth hole length. If the exclusion of this information is justified on the basis that the information is not Material and this exclusion does not detract from the understanding of the report, the Competent Person should clearly explain why this is the case.	Drill Hole Collar Information ETRS-TM35FIN projection (EPSG:3067). See body of report for the table of drill holes specifications (Table 1)
Data aggregation methods	In reporting Exploration Results, weighting averaging techniques, maximum and/or minimum grade truncations (eg cutting of high grades) and cut-off grades are usually Material and should be stated. Where aggregate intercepts incorporate short lengths of high grade results and longer lengths of low grade results, the procedure used for such aggregation should be stated and some typical examples of such aggregations should be shown in detail. The assumptions used for any reporting of metal equivalent values should be clearly stated.	A minimum sample length is 1m except at the bottom of the holes wherever possible the original surface till was samples separately to the tailings. Data has been aggregated into mineralised intercepts presented in the body of the report (Table 2). There are no short intervals of high grade. The distribution of grades are shown in Figures 2, 3 and 4 for 3 important metals or metal combinations
		No metal equivalents are used.
Relationship between mineralisation widths and intercept lengths	These relationships are particularly important in the reporting of Exploration Results. If the geometry of the mineralisation with respect to the drill hole angle is known, its nature should be reported. If it is not known and only the down hole lengths are reported, there should be a clear statement to this effect (ee 'down hole length, true width not known')	All holes were vertical and in the nature of tailings deposition the stratification is sub-horizontal
Diagrams	Appropriate maps and sections (with scales) and tabulations of intercepts should be included for any significant discovery being reported These should include, but not be limited to a plan view of drill hole collar locations and appropriate sectional views.	The location and results received for surface samples are displayed in the attached maps and/or tables. Coordinates are ETRS-TM35FIN projection (EPSG:3067).
Balanced reporting	Where comprehensive reporting of all Exploration Results is not practicable, representative reporting of both low and high grades and/or widths should be practiced to avoid misleading reporting of Exploration Results.	Histograms of assay values are reported which include the full range of values
Further work	The nature and scale of planned further work (eg tests for lateral extensions or depth extensions or large-scale step-out drilling). Diagrams clearly highlighting the areas of possible extensions, including the main geological interpretations and future drilling areas, provided this information is not commercially sensitive.	At this stage no further sampling of the TSF is envisaged. At the time of the original program 7 additional twin holes were drilled and the samples stored for later metallurgical studies